

Course No: CVL 2402  
Course Title: Foundation Engineering  
Date: 11/1/2017  
No. of Questions: (3)  
Time: 2 hr  
Using Calculator (Yes)

University of Palestine



Final Exam  
First Semester  
2016/2017  
Total Grade: 50

Instructor Name: Dr. Sari Abusharar  
Student No.: \_\_\_\_\_  
Student Name: \_\_\_\_\_  
College Name: Engineering  
Dep. / Specialist: Civil Engineering  
Using Dictionary (No)

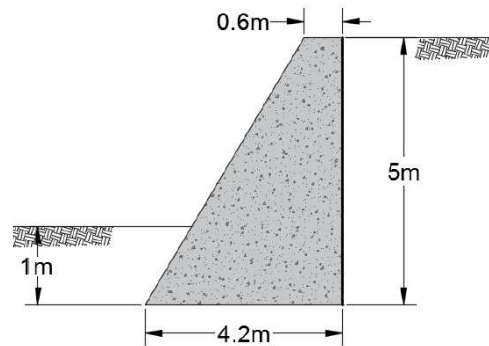
Answer All Questions

50

First Question

20/50

A gravity retaining wall shown in the figure below is required to retain 5 m of soil. The backfill is a granular soil with unit weight,  $\gamma = 18 \text{ kN/m}^3$ , and friction angle of  $\phi = 30^\circ$ . The existing soil below the base has the following properties:  $\gamma = 19 \text{ kN/m}^3$ ,  $\phi = 26^\circ$  and  $c = 40 \text{ kN/m}^2$ . The wall is embedded 1 m into the existing soil. Determine the stability (overturning, sliding, bearing capacity) of the wall assuming that there is no friction between the soil and the wall. Take  $K_1 = K_2 = 2/3$ .



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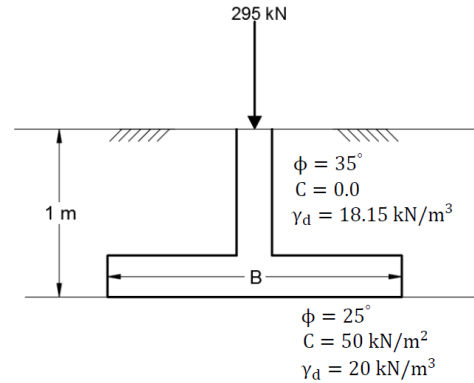
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**Second Question**

**10/50**

Determine the size of square footing to carry net allowable load of 295 kN with FS=3. Use Terzaghi equation assuming general shear failure.



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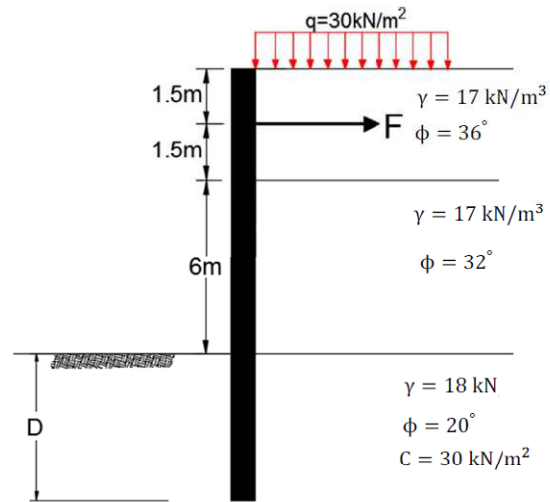
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**Third Question**

**20/50**

An anchored sheet-pile bulkhead is shown below. Use the free earth support method to:

- a. Draw the lateral earth pressure distribution with depth.
- b. Determine the theoretical depth of embedment,  $D$ .
- c. Calculate the anchor force per unit length of the sheet-pile wall.
- d. Calculate the maximum moment



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هذا الجزء خاص بالطالب الذين تغيبوا عن الامتحان النصف الثاني

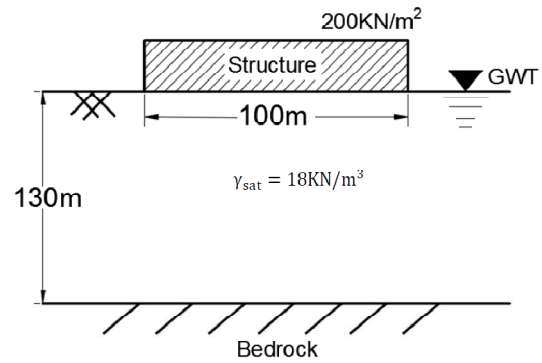
**First Question**

**15/15**

**A. Mark each of the following statements True (T) or False (F)**

1.	When the area ratio is 10% or less, the sample generally is considered to be disturbed.	
2.	A recovery ratio of unity indicates the presence of fractured rock.	
3.	Samples obtained by a thin-walled tube sampling method are less disturbed than samples obtained by split-spoon sampling method.	
4.	The net allowable bearing capacity increases by increasing the depth of embedment.	
5.	Disturbed soil samples cannot be used for consolidation, hydraulic conductivity, or shear strength tests.	

**B. Site investigation is to be made for a structure of 100 m length and 100 m width. The soil profile is shown below, if the structure is subjected to  $200 \text{ KN/m}^2$ , what is the approximate depth of borehole (Assume  $\gamma_w = 10 \text{ KN/m}^3$ ).**



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*End of Questions*  
*Good Luck*



### Useful Formulae

#### Stress Calculation using 2V:1H Method

$$\Delta\sigma = \frac{q_o \times B \times L}{(B + z)(L + z)}$$

$$q_u = 1.3c'N_c + qN_q + 0.4\gamma BN_\gamma \quad (\text{square foundation})$$

**Table 3.1** Terzaghi's Bearing Capacity Factors—Eqs. (3.4), (3.5), and (3.6) a From Kumbhojkar (1993)

$\phi'$	$N_c$	$N_q$	$N_\gamma^a$	$\phi'$	$N_c$	$N_q$	$N_\gamma^a$
0	5.70	1.00	0.00	26	27.09	14.21	9.84
1	6.00	1.10	0.01	27	29.24	15.90	11.60
2	6.30	1.22	0.04	28	31.61	17.81	13.70
3	6.62	1.35	0.06	29	34.24	19.98	16.18
4	6.97	1.49	0.10	30	37.16	22.46	19.13
5	7.34	1.64	0.14	31	40.41	25.28	22.65
6	7.73	1.81	0.20	32	44.04	28.52	26.87
7	8.15	2.00	0.27	33	48.09	32.23	31.94
8	8.60	2.21	0.35	34	52.64	36.50	38.04
9	9.09	2.44	0.44	35	57.75	41.44	45.41
10	9.61	2.69	0.56	36	63.53	47.16	54.36
11	10.16	2.98	0.69	37	70.01	53.80	65.27
12	10.76	3.29	0.85	38	77.50	61.55	78.61
13	11.41	3.63	1.04	39	85.97	70.61	95.03
14	12.11	4.02	1.26	40	95.66	81.27	115.31
15	12.86	4.45	1.52	41	106.81	93.85	140.51
16	13.68	4.92	1.82	42	119.67	108.75	171.99
17	14.60	5.45	2.18	43	134.58	126.50	211.56
18	15.12	6.04	2.59	44	151.95	147.74	261.60
19	16.56	6.70	3.07	45	172.28	173.28	325.34
20	17.69	7.44	3.64	46	196.22	204.19	407.11
21	18.92	8.26	4.31	47	224.55	241.80	512.84
22	20.27	9.19	5.09	48	258.28	287.85	650.67
23	21.75	10.23	6.00	49	298.71	344.63	831.99
24	23.36	11.40	7.08	50	347.50	415.14	1072.80
25	25.13	12.72	8.34				

<sup>a</sup>From Kumbhojkar (1993)





**Table 3.3** Bearing Capacity Factors

$\phi'$	$N_c$	$N_q$	$N_\gamma$	$\phi'$	$N_c$	$N_q$	$N_\gamma$
0	5.14	1.00	0.00	26	22.25	11.85	12.54
1	5.38	1.09	0.07	27	23.94	13.20	14.47
2	5.63	1.20	0.15	28	25.80	14.72	16.72
3	5.90	1.31	0.24	29	27.86	16.44	19.34
4	6.19	1.43	0.34	30	30.14	18.40	22.40
5	6.49	1.57	0.45	31	32.67	20.63	25.99
6	6.81	1.72	0.57	32	35.49	23.18	30.22
7	7.16	1.88	0.71	33	38.64	26.09	35.19
8	7.53	2.06	0.86	34	42.16	29.44	41.06
9	7.92	2.25	1.03	35	46.12	33.30	48.03
10	8.35	2.47	1.22	36	50.59	37.75	56.31

$$FS_{(\text{overturning})} = \frac{\sum M_R}{\sum M_o}$$

$$FS_{(\text{sliding})} = \frac{(\sum V) \tan(k_1 \phi'_2) + Bk_2 c'_2 + P_p}{P_a \cos \alpha}$$

$$FS_{(\text{bearing capacity})} = \frac{q_u}{q_{\max}}$$

$$e = \frac{B}{2} - \frac{\sum M_R - \sum M_o}{\sum V}$$

$$q_{\text{heel}}^{\text{toe}} = \frac{\sum V}{B} \left( 1 \pm \frac{6e}{B} \right)$$

$$q_u = c'_2 N_c F_{cd} F_{ci} + q N_q F_{qd} F_{qi} + \frac{1}{2} \gamma_2 B' N_\gamma F_{\gamma d} F_{\gamma i}$$

where

$$q = \gamma_2 D$$

$$B' = B - 2e$$

$$F_{cd} = F_{qd} - \frac{1 - F_{qd}}{N_c \tan \phi'_2}$$

$$F_{qd} = 1 + 2 \tan \phi'_2 (1 - \sin \phi'_2)^2 \frac{D}{B'}$$

$$F_{\gamma d} = 1$$

$$F_{ci} = F_{qi} = \left( 1 - \frac{\psi^\circ}{90^\circ} \right)^2$$

$$F_{\gamma i} = \left( 1 - \frac{\psi^\circ}{\phi'_2} \right)^2$$

$$\psi^\circ = \tan^{-1} \left( \frac{P_a \cos \alpha}{\sum V} \right)$$